

EEXI Technical File(EPL)

Ship's name: DONG FANG FU(东方富)

IMO No.: 9162423

Company: Fujian Orient Shipping Co., Ltd.

Concents

1	Data-----	3
1.1	General information-----	3
1.2	Principal particulars-----	3
1.3	Main engine-----	3
1.4	Auxiliary engine-----	3
1.5	Ship speed-----	4
2	Power curve-----	5
3	Overview of propulsion system and electric power supply system-----	6
3.1	Propulsion system-----	6
3.1.1	Main engine-----	6
3.1.2	Propeller-----	6
3.2	Electric power supply system-----	6
3.2.1	Auxiliary engines-----	6
3.2.2	Main generators-----	6
4	Estimation process of speed-power curve-----	7
5	Description of energy saving equipment-----	7
6	Calculated value of attained EEXI-----	7
6.1	Basic data-----	7
6.2	Main engine-----	8
6.3	Auxiliary engines-----	8
6.4	Ice class-----	9
6.5	Innovative electrical energy efficient technology-----	9
6.6	Innovative mechanical energy efficient technology-----	9
6.7	f_j -----	9
6.8	f_i -----	9
6.9	f_c -----	9
6.10	f_l -----	9
6.11	f_w -----	10
6.12	f_m -----	10
6.13	Calculated value of attained EEXI-----	11
6.14	Calculated value of required EEXI-----	11
7	EPL table-----	12

1 Data

1.1 General information

Shipowner	Fujian Orient Shipping Co., Ltd.
Shipbuilder	Imabari Shipbuilding Co., Ltd.
Hull no.	538
IMO no.	9162423
Ship type	Container ship

1.2 Principal particulars

Length overall	161.85 m
Length between perpendiculars	150 m
Breadth, moulded	25.6 m
Depth, moulded	12.9 m
Summer load line draught, moulded	9.07 m
Deadweight at summer load line draught	18185 tons

1.3 Main engine

Manufacturer	MITSUI ENGINEERING & SHIPPING CO.,LTD
Type	7S50MC
Maximum continuous rating (MCR_{Me})	9988 kW
Limited maximum continuous rating with the Engine Power Limitation installed ($MCR_{ME,lim}$)	7426 kW
SFC at 75% of MCR_{me}	190 g/kWh
Number of sets	1
Fuel type	HFO

1.4 Auxiliary engine

Manufacturer	YANMAR DIESEL ENGINE CO.,LTD
Type	M220AL-UN

Maximum continuous rating (MCR_{AE})	736 kW
SFC at 50% MCR_{AE}	215 g/kWh
Number of sets	3
Fuel type	HFO

1.5 Ship speed

Ship speed (V_{ref}) (with the Engine Power Limitation installed)	16.16 knots
---	-------------

2 Power curve

The speed-power curve is not available, the ship speed V_{ref} is approximated by $V_{ref,app}$ which is obtained from statistical mean of distribution of ship speed and engine power as below:

$$V_{ref,avg} = A \times B^c = 3.2395 \times 18185.0^{0.18294} = 19.487222$$

$$MCR_{avg} \text{ or } MPP_{avg} = D \times E^F = 0.5042 \times 18185.0^{1.03046} = 12361.381616$$

m_v is a performance margin of a ship, which should be 5% of $V_{ref,avg}$ or one knot, whichever is lower;

$$m_v = 0.974361$$

$$\begin{aligned} V_{ref,app} &= (V_{ref,avg} - m_v) \times \left[\frac{\sum P_{ME}}{0.75 \times MCR_{avg}} \right]^{\frac{1}{3}} \\ &= (19.487222 - 0.974361) \times \left[\frac{6,164}{0.75 \times 12361.381616} \right]^{\frac{1}{3}} \\ &= 16.16[\text{knot}] \end{aligned}$$

3 Overview of propulsion system and electric power supply system

3.1 Propulsion system

3.1.1 Main engine

Refer to paragraph 1.3 of this file.

3.1.2 Propeller

Type	Fixed pitch propeller
Diameter	5460
Number of blades	5
Number of set	1

3.2 Electric power supply system

3.2.1 Auxiliary engines

Refer to paragraph 1.4 of this file.

3.2.2 Main generators

Manufacturer	NISHISIBA ELECTRIC CO.,LTD
Rated output	680
Voltage	450
Number of set	3

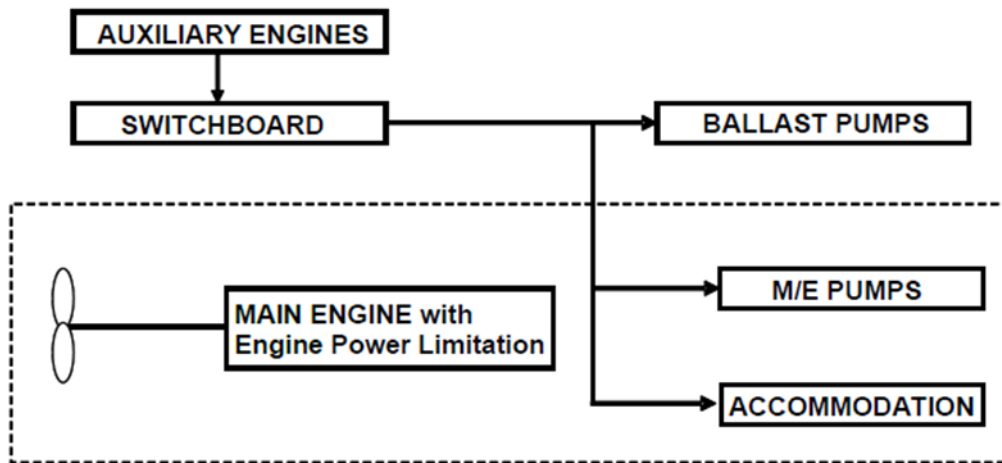


Figure 3.1: Schematic figure of propulsion and electric power supply system

4 Estimation process of speed-power curve

N/A

5 Description of energy saving equipment

5.1 Energy saving equipment the effects of which are expressed as $P_{AEff(i)}$ or $P_{eff(i)}$ in the EEXI calculation formula

N/A

5.2 Other energy saving equipment

N/A

6 Calculated value of attained EEXI

6.1 Basic data

Type of ship	Capacity DWT	Speed V_{ref} (knots)
Container ship	12,730	16.16

6.2 Main engine

MCR_{ME} (kW)	$MCR_{ME,lim}$ (kW)	P_{ME} (kW)	Type of fuel	C_{FME}	SFC_{ME} (g/kWh)
9988	7426	6164	HFO	3.114	190

Where:

$$P_{ME}=83\%MCR_{ME,lim}=6,164 \text{ (kW)}$$

The following defaults are used in the calculation:

Type of fuel: HFO

C_{FME} : 3.114

SFC_{ME} : 190 (g/kWh)

6.3 Auxiliary engines

P_{AE} (kW)	Type of fuel	C_{FAE}	SFC_{AE} (g/kWh)
499	HFO	3.114	215

Where:

$$\sum_{i=1}^{n_{PTI}} P_{PTI(i)} = 0$$

$$\begin{aligned} P_{AE} &= 0.05 \times \left(\sum_{i=1}^{n_{ME}} MCR_{ME(i)} + \frac{\sum_{i=1}^{n_{PTI}} P_{PTI(i)}}{0.75} \right) \\ &= 0.05 \times \left(9988 + \frac{0}{0.75} \right) \\ &= 499 \text{ (kW)} \end{aligned}$$

SFC_{AE} :

No.	$MCR_{AE(i)}$ (kW)	$SFC_{AE(i)}$ (g/kWh)
1	736	215
2	736	215
3	736	215

$$\begin{aligned} SFC_{AE} &= \frac{\sum_{i=1}^{n_{AE}} (MCR_{AE(i)} \times SFC_{AE(i)})}{\sum_{i=1}^{n_{AE}} MCR_{AE(i)}} \\ &= \frac{736 \times 215 + 736 \times 215 + 736 \times 215}{736 + 736 + 736} \\ &= 215 \text{ [g/kWh]} \end{aligned}$$

6.4 Ice class

Ice class:N/A

6.5 Innovative electrical energy efficient technology

Peff:N/A

6.6 Innovative mechanical energy efficient technology

PAEff:N/A

6.7 f_j

$$f_j = 1$$

6.8 f_i

$$f_i = 1$$

6.9 f_c

f_c is the cubic capacity correction factor and should be assumed to be one (1.0) if no necessity of the factor is granted.

$$f_c = 1$$

6.10 f_l

$f_{cranes} = 1$ If no cranes are present.

$f_{sideloader} = 1$ If no side loaders are present.

$f_{RoRo} = 1$ If no ro-ro ramp is present.

$$f_l = f_{cranes} \times f_{sideloader} \times f_{RoRo} = 1$$

6.11 f_w

$$f_w = 1$$

6.12 f_m

If ice class ship with notation "IA Super" or "IA", then $f_m=1.05$, else $f_m= 1$;

$$f_m = 1$$

6.13 Calculated value of attained EEXI

$$\begin{aligned}
 EEXI &= \frac{(\prod_{j=1}^M f_j)(\sum_{i=1}^{nME} P_{ME(i)} \cdot C_{FME(i)} \cdot SFC_{ME(i)}) + (P_{AE} \cdot C_{FAE} \cdot SFC_{AE})}{f_i \cdot f_c \cdot f_l \cdot Capacity \cdot f_w \cdot V_{ref} \cdot f_m} \\
 &+ \frac{\{(\prod_{j=1}^M f_j \cdot \sum_{i=1}^{nPTI} P_{PTI(i)} - \sum_{i=1}^{neff} f_{eff(i)} \cdot P_{AE_{eff(i)}})\} \cdot C_{FAE} \cdot SFC_{AE}}{f_i \cdot f_c \cdot f_l \cdot Capacity \cdot f_w \cdot V_{ref} \cdot f_m} \\
 &- \frac{(\sum_{i=1}^{neff} f_{eff(i)} \cdot P_{eff(i)} \cdot C_{FME} \cdot SFC_{ME})}{f_i \cdot f_c \cdot f_l \cdot Capacity \cdot f_w \cdot V_{ref} \cdot f_m} \\
 &= \frac{1 \times (6164 \times 3.114 \times 190) + (499 \times 3.114 \times 215)}{1 \times 1 \times 1 \times 12730 \times 1 \times 16.16 \times 1} \\
 &+ \frac{\{(1 \times 0 - 0 \times 0 \times 3.114) \times 215\}}{1 \times 1 \times 1 \times 12730 \times 1 \times 16.16 \times 1} \\
 &- \frac{(0 \times 0 \times 3.114 \times 190)}{1 \times 1 \times 1 \times 12730 \times 1 \times 16.16 \times 1} \\
 &= 19.4(g - CO_2/ton \cdot mile)
 \end{aligned}$$

Attained EEXI: 19.4 g-CO₂/ton mile

6.14 Calculated value of required EEXI

The reference line value RLV is calculated as follows:

$$RLV = a \times b^{(-c)} = 174.22 \times 18185.0^{-0.201} = 24.2603$$

The required EEXI is calculated as follows:

$$\begin{aligned}
 \text{Required EEXI} &= (1-y/100) \times RLV \\
 &= (1-20/100) \times 24.2603 \\
 &= 19.4 \text{ (g-CO}_2\text{/ton}\cdot\text{mile)}
 \end{aligned}$$

Where, y=20, is the reduction factor

Required EEXI: 19.4 g-CO₂/ton mile

Attained EEXI ≤ Required EEXI

7 EPL table

Current					With EPL						
MCR (kW)	Vref (knot)	Req.EEXI (g-CO ₂ /ton mile)	Att.EEXI (g-CO ₂ /ton mile)	EEXI Deviation	▽EPL	MCR _{lim} (kW)	De-rated MCR	Vref (knot)	Att.EEXI (g-CO ₂ /ton mile)	EEXI Deviation	Improved EEXI
9988	17.24	19.4	21.7	11.86%	-999	8989	-10%	17.22	21.7	11.86%	+0%
9988	17.24	19.4	21.7	11.86%	-2562	7426	-26%	16.16	19.4	0.0%	+11%
9988	17.24	19.4	21.7	11.86%	-2996	6992	-30%	15.84	18.7	-3.61%	+14%
9988	17.24	19.4	21.7	11.86%	-3496	6492	-35%	15.45	17.9	-7.73%	+18%