

# **EEFI Technical File(EPL)**

**Ship's name: DONG FANG QIANG(东方强)**

**IMO No.: 9122538**

**Company: Fujian Orient Shipping Co., Ltd.**

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# 1 Data

## 1.1 General information

Shipowner	Fujian Orient Shipping Co., Ltd.
Shipbuilder	Flensburger Schiffbau GmbH & Co.,KG Germany
Hull no.	692
IMO no.	9122538
Ship type	Container ship

## 1.2 Principal particulars

Length overall	174.36 m
Length between perpendiculars	163.52 m
Breadth, moulded	30.6 m
Depth, moulded	16 m
Summer load line draught, moulded	11.87 m
Deadweight at summer load line draught	32483 tons

## 1.3 Main engine

Manufacturer	MANISES DIESEL ENGINE
Type	MAN B&W 6S70MC
Maximum continuous rating ( $MCR_{Me}$ )	16846 kW
Limited maximum continuous rating with the Engine Power Limitation installed ( $MCR_{ME,lim}$ )	13495 kW
SFC at 75% of $MCR_{me}$	190 g/kWh
Number of sets	1
Fuel type	HFO

## 1.4 Auxiliary engine

Manufacturer	YANMAR DIESEL ENGINE
Type	6N260L-SN

Maximum continuous rating ( $MCR_{AE}$ )	1214 kW
SFC at 50% $MCR_{AE}$	215 g/kWh
Number of sets	3
Fuel type	HFO

## 1.5 Ship speed

Ship speed ( $V_{ref}$ ) (with the Engine Power Limitation installed)	18.04 knots
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## 2 Power curve

The speed-power curve is not available, the ship speed  $V_{ref}$  is approximated by  $V_{ref,app}$  which is obtained from statistical mean of distribution of ship speed and engine power as below:

$$V_{ref,avg} = A \times B^c = 3.2395 \times 32483.0^{0.18294} = 21.669074$$

$$MCR_{avg} \text{ or } MPP_{avg} = D \times E^F = 0.5042 \times 32483.0^{1.03046} = 22474.188505$$

$m_v$  is a performance margin of a ship, which should be 5% of  $V_{ref,avg}$  or one knot, whichever is lower;

$$m_v = 1$$

$$\begin{aligned} V_{ref,app} &= (V_{ref,avg} - m_v) \times \left[ \frac{\sum P_{ME}}{0.75 \times MCR_{avg}} \right]^{\frac{1}{3}} \\ &= (21.669074 - 1) \times \left[ \frac{11,201}{0.75 \times 22474.188505} \right]^{\frac{1}{3}} \\ &= 18.04[knot] \end{aligned}$$

### 3 Overview of propulsion system and electric power supply system

#### 3.1 Propulsion system

##### 3.1.1 Main engine

Refer to paragraph 1.3 of this file.

##### 3.1.2 Propeller

Type	
Diameter	
Number of blades	
Number of set	

#### 3.2 Electric power supply system

##### 3.2.1 Auxiliary engines

Refer to paragraph 1.4 of this file.

##### 3.2.2 Main generators

Manufacturer	NISHISHIBA ELECTRIC CO.,LTD
Rated output	1100
Voltage	450
Number of set	3

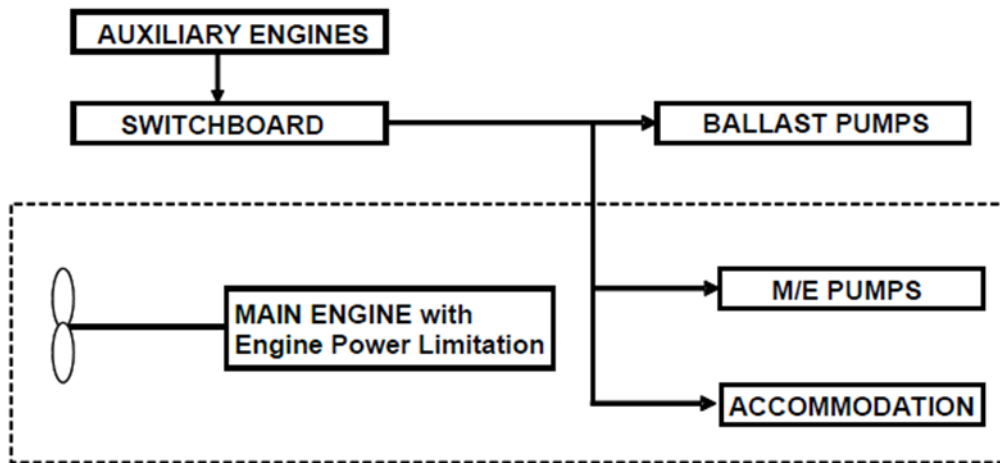


Figure 3.1: Schematic figure of propulsion and electric power supply system

#### 4 Estimation process of speed-power curve

N/A

#### 5 Description of energy saving equipment

5.1 Energy saving equipment the effects of which are expressed as  $P_{AEff(i)}$  or  $P_{eff(i)}$  in the EEXI calculation formula

N/A

5.2 Other energy saving equipment

N/A

#### 6 Calculated value of attained EEXI

##### 6.1 Basic data

Type of ship	Capacity DWT	Speed $V_{ref}$ (knots)
Container ship	22,738	18.04

## 6.2 Main engine

$MCR_{ME}$ (kW)	$MCR_{ME,lim}$ (kW)	$P_{ME}$ (kW)	Type of fuel	$C_{FME}$	$SFC_{ME}$ (g/kWh)
16846	13495	11201	HFO	3.114	190

Where:

$$P_{ME}=83\%MCR_{ME,lim}=11,201 \text{ (kW)}$$

The following defaults are used in the calculation:

Type of fuel: HFO

$C_{FME}$ : 3.114

$SFC_{ME}$ : 190 (g/kWh)

## 6.3 Auxiliary engines

$P_{AE}$ (kW)	Type of fuel	$C_{FAE}$	$SFC_{AE}$ (g/kWh)
671	HFO	3.114	215

Where:

$$\sum_{i=1}^{n_{PTI}} P_{PTI(i)} = 0$$

$$P_{AE} = \left\{ 0.025 \times \left( \sum_{i=1}^{n_{ME}} MCR_{ME(i)} + \frac{\sum_{i=1}^{n_{PTI}} P_{PTI(i)}}{0.75} \right) \right\} + 250$$

$$= \left\{ 0.025 \times \left( 16846 + \frac{0}{0.75} \right) \right\} + 250$$

$$= 671 \text{ (kW)}$$

$SFC_{AE}$ :

No.	$MCR_{AE(i)}$ (kW)	$SFC_{AE(i)}$ (g/kWh)
1	1214	215
2	1214	215
3	1214	215

$$SFC_{AE} = \frac{\sum_{i=1}^{n_{AE}} (MCR_{AE(i)} \times SFC_{AE(i)})}{\sum_{i=1}^{n_{AE}} MCR_{AE(i)}}$$

$$= \frac{1214 \times 215 + 1214 \times 215 + 1214 \times 215}{1214 + 1214 + 1214}$$

$$= 215 \text{ [g/kWh]}$$



## 6.4 Ice class

Ice class:N/A

## 6.5 Innovative electrical energy efficient technology

Peff:N/A

## 6.6 Innovative mechanical energy efficient technology

PAEff:N/A

## 6.7 $f_j$

$$f_j = 1$$

## 6.8 $f_i$

$$f_i = 1$$

## 6.9 $f_c$

$f_c$  is the cubic capacity correction factor and should be assumed to be one (1.0) if no necessity of the factor is granted.

$$f_c = 1$$

## 6.10 $f_l$

$f_{cranes} = 1$  If no cranes are present.

$f_{sideloader} = 1$  If no side loaders are present.

$f_{RoRo} = 1$  If no ro-ro ramp is present.

$$f_l = f_{cranes} \times f_{sideloader} \times f_{RoRo} = 1$$

### 6.11 $f_w$

$$f_w = 1$$

### 6.12 $f_m$

If ice class ship with notation "IA Super" or "IA", then  $f_m=1.05$ , else  $f_m= 1$ ;

$$f_m = 1$$

### 6.13 Calculated value of attained EEXI

$$\begin{aligned}
 EEXI &= \frac{(\prod_{j=1}^M f_j)(\sum_{i=1}^{nME} P_{ME(i)} \cdot C_{FME(i)} \cdot SFC_{ME(i)}) + (P_{AE} \cdot C_{FAE} \cdot SFC_{AE})}{f_i \cdot f_c \cdot f_l \cdot Capacity \cdot f_w \cdot V_{ref} \cdot f_m} \\
 &+ \frac{\{(\prod_{j=1}^M f_j \cdot \sum_{i=1}^{nPTI} P_{PTI(i)} - \sum_{i=1}^{neff} f_{eff(i)} \cdot P_{AE_{eff(i)}})\} \cdot C_{FAE} \cdot SFC_{AE}}{f_i \cdot f_c \cdot f_l \cdot Capacity \cdot f_w \cdot V_{ref} \cdot f_m} \\
 &- \frac{(\sum_{i=1}^{neff} f_{eff(i)} \cdot P_{eff(i)} \cdot C_{FME} \cdot SFC_{ME})}{f_i \cdot f_c \cdot f_l \cdot Capacity \cdot f_w \cdot V_{ref} \cdot f_m} \\
 &= \frac{1 \times (11201 \times 3.114 \times 190) + (671 \times 3.114 \times 215)}{1 \times 1 \times 1 \times 22738 \times 1 \times 18.04 \times 1} \\
 &+ \frac{\{(1 \times 0 - 0 \times 0 \times 3.114) \times 215\}}{1 \times 1 \times 1 \times 22738 \times 1 \times 18.04 \times 1} \\
 &- \frac{(0 \times 0 \times 3.114 \times 190)}{1 \times 1 \times 1 \times 22738 \times 1 \times 18.04 \times 1} \\
 &= 17.3(g - CO_2/ton \cdot mile)
 \end{aligned}$$

**Attained EEXI: 17.3 g-CO<sub>2</sub>/ton mile**

### 6.14 Calculated value of required EEXI

The reference line value RLV is calculated as follows:

$$RLV = a \times b^{(-c)} = 174.22 \times 32483.0^{-0.201} = 21.5901$$

The required EEXI is calculated as follows:

$$\begin{aligned}
 \text{Required EEXI} &= (1-y/100) \times RLV \\
 &= (1-20/100) \times 21.5901 \\
 &= 17.3 \quad (\text{g-CO}_2/\text{ton} \cdot \text{mile})
 \end{aligned}$$

Where, y=20, is the reduction factor

**Required EEXI: 17.3 g-CO<sub>2</sub>/ton mile**

**Attained EEXI ≤ Required EEXI**

## 7 EPL table

Current					With EPL						
MCR (kW)	Vref (knot)	Req.EEXI (g-CO <sub>2</sub> /ton mile)	Att.EEXI (g-CO <sub>2</sub> /ton mile)	EEXI Deviation	▽EPL	MCR <sub>lim</sub> (kW)	De-rated MCR	Vref (knot)	Att.EEXI (g-CO <sub>2</sub> /ton mile)	EEXI Deviation	Improved EEXI
16846	18.78	17.3	18.6	7.51%	-1685	15161	-10%	18.75	18.5	6.94%	+1%
16846	18.78	17.3	18.6	7.51%	-3351	13495	-20%	18.04	17.3	0.0%	+7%
16846	18.78	17.3	18.6	7.51%	-4211	12635	-25%	17.65	16.6	-4.05%	+11%
16846	18.78	17.3	18.6	7.51%	-5054	11792	-30%	17.24	15.9	-8.09%	+15%